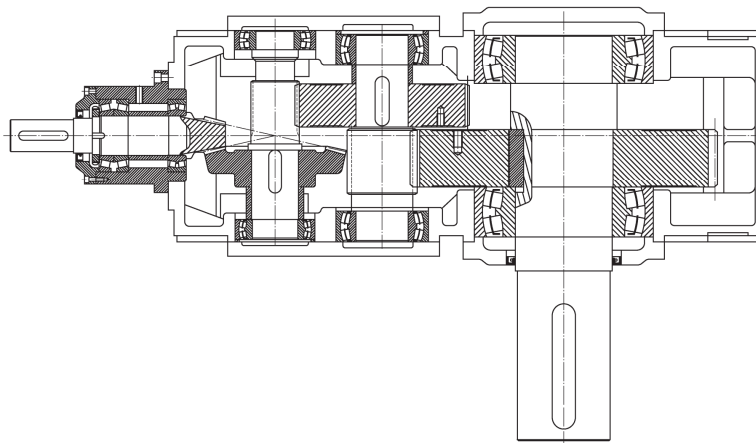


H、B series gear units overview:

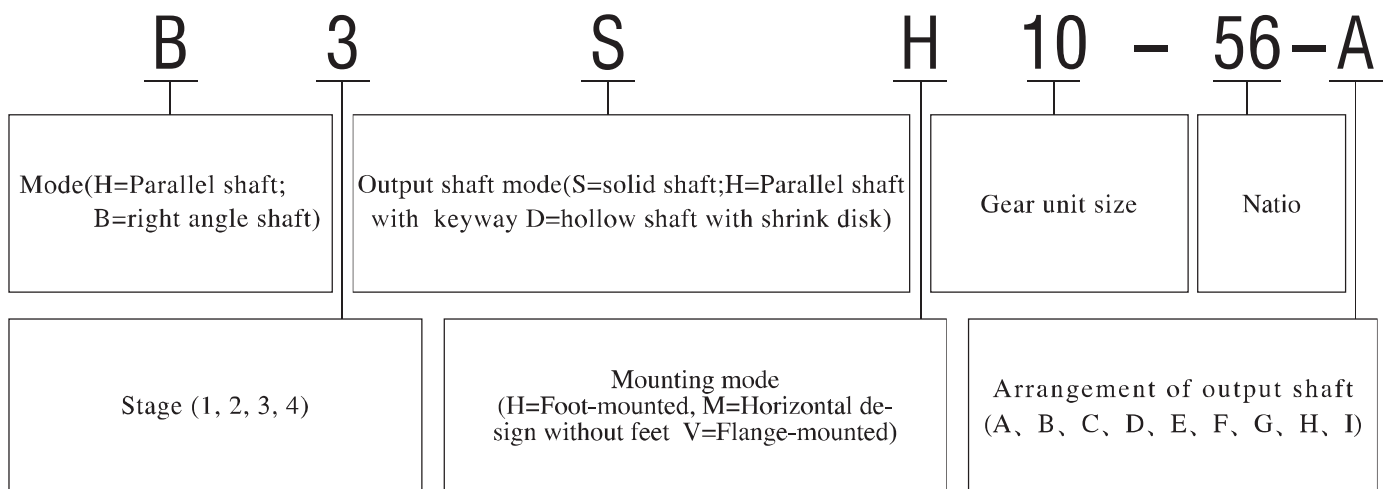
- ❑ H.B series gear units adopt currency layout and may transform into speeral reducer according to customer's requirement.
- ❑ The housing of one size can realize parallel shaft,right-angle shaft modes and horizontal,vertical mounting modes.Variety of components is reducible, the number of reducer's mode is augmentable.
- ❑ Sound-absorbable structure, lager surface, big fan reduce temperature and noise, advanced grinding process of cylindrical gear and bevel gear improve stability and transmit power more efficeintly.
- ❑ Input mode: motor connected flange, shaft input.
- ❑ Output mode: solid shaft with flat key, hollow shaft with flat key, hollow shaft with shrink disk, hollow or solid shaft with involute splines, solid shaft with flange.
- ❑ Mounting mode: Foot-mounted, flange-mounted, swing base-mounted, torque-arm-mounted.
- ❑ H.B series include sizes 3~26, number of stages is 1~4, ratio is 1.25~450, combining with R series and K series, ratio will be higher.

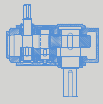
H.B series reducer structure drawing:



HB

H.B series model expressing example:





Symbol description:

ED=operating cycle per hour, express as

percent, for example ED=60%/h

f1=Factor for driven machine (table 1)

f2=Factor for prime mover

f3=Peak torque factor

f4,f5=Ambient temperature factor (table 2,3)

f6,f7=Altitude factor (table 4,5)

f8=Applying oil factor of gear box (table 6)

f9,f10,f11,f12=Thermal capacity factor (table 7,8,9,10)

a1=Size factor (table 11)

a2=Transmission ratio factor (table 12)

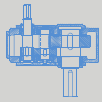
P1=Power rating of driven machine

PG1=Thermal capacity for gear units without auxiliary
cooling,

PG2=Thermal capacity for gear units with fan cooling,

PG3=Thermal capacity for gear units with built-in cooling
coil

PG4=Thermal capacity for gear units with built-in cooling
coil and fan

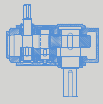


HB series type selection example:

Steps	Specification	Symbol	Calculate parameter					
1	Driven machine factor	f_1	See P05 f_1 table					
2	Factor for prime mover	f_2	Factor for prime mover			f_2		
			Electric motors, hydraulic motors, turbines			1.0		
			Piston engines 4 - 6 cylinders cyclic variation 1 : 100 to 1 : 200			1.25		
			Piston engines 1 - 3 cylinders cyclic variation up to 1 : 100			1.5		
3	Permissible input speed	n_1	≤ 1500					
4	Position of input and output	H、 B	H:Parallel shaft, B: Right-angled shaft.					
5	Determine ration	i	$i=n_1/n_2$					
6	Efficiency	η	single stage:98%, 2-stage:96%, 3-stage:94%, 四级4-stage:92%					
7	Determine input power	P_1	$P_1=T_2 \cdot n_1/(9550 \cdot i \cdot \eta)$ or $P_1=P_2/\eta$					
8	By calculation, determine type in reference to transmission table	T_2N 、 P_{1N}	$T_2N \geq T_2 \cdot f_1 \cdot f_2$ (or) $P_{1N} \geq P_1 \cdot f_1 \cdot f_2$ If not meet: $3.33 \cdot P_1 \geq P_{1N}$ please consult us.					
9	Determine output mode		Output mode & mounting position					
10	Check for maximum torque	T_A	$P_{1N} \geq T_A \cdot n_1 \cdot f_3/9550$	f_3	Load peaks per hour			
					1-5	6-30	31-100	> 100
				Steady direction of load	0.5	0.65	0.7	0.85
Alternating direction of load	0.7	0.95	1.10	1.25				
11	Verify intensity of shaft	F_r 、 F_a	See P05					
12	Determine lubrication method and lubrication oil(see attachment)		Horizontal		Vertical			
			Immersion, splash, forced lubrication.		A: immersion B: Pump-forced lubrication			
13	Cooling method		1 Adequate for gear units without auxiliary cooling, if: $P_1 \leq PG_1 \times f_4 \times f_6 \times f_8 \times f_9$ 2 Adequate for gear units with fan cooling, if: $P_1 \leq PG_2 \times f_4 \times f_6 \times f_8 \times f_{10}$ 3 Adequate for gear units with fitted cooling coil, if: $P_1 \leq PG_3 \times f_5 \times f_7 \times f_8 \times f_{11}$ 4 Adequate for gear units with cooling coil and fan, if: $P_1 \leq PG_4 \times f_5 \times f_7 \times f_8 \times f_{12}$ 5 For higher thermal capacities, cooling by external oil cooler on request: (f_4 、 f_5 、 f_6 、 f_7 、 f_8 、 f_9 、 f_{10} 、 f_{11} 、 f_{12} refer to P213,214)					

HB

* Peak torque: Maximum torque is maximum starting torque, maximum braking torque.



Selection example

Given condition:

Driving machine:

$P_m=75\text{KW}$
 $n_1=1500\text{rpm}$
 $T_A=720\text{N} \cdot \text{m}$

Driven machine(belt conveyor):

$P_2=66\text{KW}$
 $n_2=26\text{rpm}$
service duration: 12h/day
Start-up: 10times/hour
Working circle ED=100% per hour
Ambient temperature: 30°C
installed in open field
Altitude: 500m
Right-angled shaft
Mounting mode: Horizontal
Shaft amangement: C

Selecting steps:

1.Calculate ratio:

$$i=n_1/n_2=1500/26=57.7 \quad i_N=56$$

2.Determine nominal power:

$$P_{1N} \geq P_1 \cdot f_1 \cdot f_2 = P_2 \cdot f_1 \cdot f_2 / \eta$$
$$= 66 \times 1.3 \times 1/0.94 = 91.3\text{kW}$$

Choose B3, size: 9, P_{1N} : 96kW

$$\text{Verify: } 3.33 \times P_1 \geq P_{1N}$$

$$3.33 \times P_1 = 3.33 \times P_2 / \eta = 3.33 \times 66 / 0.94$$
$$= 233.8 \text{ kW} > P_{1N}$$

3.Verify peak torque:

$$P_{iN} \geq T_A \cdot n_1 \cdot f_3 / 9550$$
$$= 720 \times 1500 \times 0.65 / 9550 = 73.5\text{kW}$$

$P_{1N}=96\text{kW} > 73.5\text{kW}$ Meet requirement.

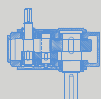
4.Verify thermal capacity:

$$P_{G1} \times f_4 \times f_6 \times f_8 \times f_9$$
$$= 70.7\text{kW} \times 0.88 \times 1 \times 1 \times (1.23-2.80 \times 0.085 \times 0.15)$$
$$= 74.3\text{kW}$$

$$P_1 = P_2 / \eta = 66\text{kW} / 0.94 = 70.2 < 74.3\text{kW}$$

So auxiliary cooling devece is unnecessary.

TYPE: B3SH9-56-C



Service Factors

Table 1		Factor for driven machine			f ₁		
Driven machines	Effective daily operating period under load in hours			Driven machines	Effective daily operating period under load in hours		
	0.5	>0.5-10	>10		0.5	>0.5-10	>10
Waste water treatment				Conveyors			
Thickeners (central drive)	-	-	1.2	Bucket conveyors	-	1.4	1.5
Filter presses	1.0	1.3	1.5	Hauling winches	1.4	1.6	1.6
Flocculation apparatus	0.8	1.0	1.3	Hoists	-	1.5	1.8
Aerators	-	1.8	2.0	Belt conveyors 150 kW	1.0	1.2	1.3
Raking equipment	1.0	1.2	1.3	Belt conveyors 150 kW	1.1	1.3	1.4
Combined longitudinal and rotary rakes	1.0	1.3	1.5	Goods lifts	-	1.2	1.5
Pre-thickeners	-	1.1	1.3	Passenger lifts	-	1.5	1.8
Screw pumps	-	1.3	1.5	Apron conveyors	-	1.2	1.5
Water turbines	-	-	2.0	Escalators	1.0	1.2	1.4
Pumps				Rail travelling gears	-	1.5	-
Centrifugal pumps	1.0	1.2	1.3	Frequency converters	-	1.8	2.0
Positive-displacement pumps				Reciprocating compressors	-	1.8	2.0
1 piston	1.3	1.4	1.8	Cranes			
> 1piston	1.2	1.4	1.5	Slewing gears	1.0	1.4	1.8
Dredgers				Luffing gears	1.0	1.1	1.4
Bucket conveyors	-	1.6	1.6	Travelling gears	1.1	1.6	2.0
Dumping devices	-	1.3	1.5	Hoisting gears	1.0	1.1	1.4
Caterpillar travelling gears	1.2	1.6	1.8	Derricking jib cranes	1.0	1.2	1.6
Bucket wheel excavators				Cooling towers			
as pick-up	-	1.7	1.7	Cooling tower fans	-	-	2.0
for primitive material	-	2.2	2.2	Blowers (axial and radial)	-	1.4	1.5
Cutter heads	-	2.2	2.2	Food industry			
Traversing gears	-	1.4	1.8	Cane sugar production			
Plate bending machines	-	1.0	1.0	Cane knives	-	-	1.7
Chemical industry				Cane mills	-	-	1.7
Extruders	-	-	1.6	Beet sugar production			
Dough mills	-	1.8	1.8	Beet cassettes macerators,	-	-	1.2
Rubber calenders	-	1.5	1.5	Extraction plants, Mechanical			
Cooling drums	-	1.3	1.4	refrigerators, Juice boilers,	-	-	1.4
Mixers for				Sugar beet washing machines,			
uniform media	1.0	1.3	1.4	Sugar beet cutters	-	-	1.5
non-uniform media	1.4	1.6	1.7	Paper machines			
Agitators for media with				of all-kind	-	1.8	2.0
uniform density	1.0	1.3	1.5	Pulper drives	On request		
non-uniform density	1.2	1.4	1.6	Centrifugal compressors	-	1.4	1.5
non-uniform gas absorption	1.4	1.6	1.8	Cableways			
Toasters	1.0	1.3	1.5	Material ropeways	-	1.3	1.4
Centrifuges	1.0	1.2	1.3	To- and fro system			
Metal working mills				aerial ropeways	-	1.6	1.8
Plate tilters	1.0	1.0	1.2	T-bar lifts	-	1.3	1.4
Ingot pushers	1.0	1.2	1.2	Continuous ropeways	-	1.4	1.6
Winding machines	-	1.6	1.6	Cement industry			
Cooling bed transfer frames	-	1.5	1.5	Concrete mixers	-	1.5	1.5
Roller straighteners	-	1.6	1.6	Breakers	-	1.2	1.4
Roller tables				Rotary kilns	-	-	2.0
continuous	-	1.5	1.5	Tube mills	-	-	2.0
intermittent	-	2.0	2.0	Separators	-	1.6	1.6
Reversing tube mills	-	1.8	1.8	Roll crushers	-	-	2.0
Shears							
continuous	-	1.5	1.5				
crank type	1.0	1.0	1.0				
Continuous casting drivers	-	1.4	1.4				
Rolls							
Reversing blooming mills	-	2.5	2.5				
Reversing slabbing mills	-	2.5	2.5				
Reversing wire mills	-	1.8	1.8				
Reversing sheet mills	-	2.0	2.0				
Reversing plate mills	-	1.8	1.8				
Roll adjustment drives	0.9	1.0	-				

1. Design for power rating of driven machine P₂

*) Designed power corresponding to max. torque

**) Load can be exactly classified, for Instance.

***) A check for thermal capacity is absolutely essential

2. The listed factors are empirical values. Prerequisite for their application is that the machinery and equipment mentioned correspond to generally accepted design and load specifications. In case of deviations from standard conditions, please refer to us.

3. For driven machines which are not listed in this table, please refer to us.

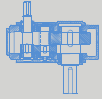


Table 2 Thermal factor f4					
Without auxiliary cooling or with fan cooling					
Ambient temperature	Operating cycle per hour (ED) in %				
	100	80	60	40	20
10 °C	1.11	1.31	1.60	2.14	3.64
20 °C	1.00	1.18	1.44	1.93	3.28
30 °C	0.88	1.04	1.27	1.70	2.89
40 °C	0.75	0.89	1.08	1.45	2.46
50 °C	0.63	0.74	0.91	1.22	2.07

Table 4 Factor for altitude f6					
Without auxiliary cooling or with fan cooling					
Factor	Altitude (metres above MSL)				
	up to 1000	up to 2000	up to 3000	up to 4000	up to 5000
f6	1.0	0.95	0.90	0.85	0.80

Table 3 Thermal factor f5					
For cooling with cooling coil, or with fan and cooling coil					
Ambient temperature	Operating cycle per hour (ED) in %				
	100	80	60	40	20
10 °C	1.05	1.23	1.50	2.03	3.41
20 °C	1.00	1.17	1.43	1.93	3.25
30 °C	0.93	1.09	1.33	1.79	3.02
40 °C	0.87	1.02	1.24	1.68	2.83
50 °C	0.81	0.95	1.16	1.56	2.63

Table 5 Factor for altitude f7					
For cooling with cooling coil, or with fan and cooling coil					
Factor	Altitude (metres above MSL)				
	up to 1000	up to 2000	up to 3000	up to 4000	up to 5000
f7	1.0	0.98	0.96	0.94	0.92

Table 6 Oil supply factor for vertical gear units. For horizontal gear units $f_8 = 1.0$, and in case of forced lubrication $f_8 = 1.05$ f8									
Gear unit type	Oil supply	Sizes 4 ... 12			Sizes 13 ... 18				
		Without auxiliary cooling	With fan	With cooling coil	With fan and cooling coil	Without auxiliary cooling	With fan	With cooling coil	With fan and cooling coil
H2.V, H3.V H4.V	Dip lubrication	0.95	*	0.95	*	*	*	*	*
	Forced lubrication	1.15	*	1.05	*	1.15	*	1.05	*
B2.V, B3.V B4.V	Dip lubrication	0.95	0.95	0.95	0.95	*	*	*	*
	Forced lubrication	1.15	1.10	1.10	1.10	1.15	1.10	1.10	1.10

Table 7 Thermal capacity factor for gear units without auxiliary cooling f9				
Gear unit type	n 1/min	Place of installation		
		Small confined spaces Wind velocity ≥ 0.5 m/s	Large halls, workshops Wind velocity ≥ 1.4 m/s	In the open Wind velocity ≥ 4.0 m/s
H1	750	$0.68 - 0.26 \times a_1 \times a_2$	$0.79 - 0.27 \times a_1 \times a_2$	1.00
	1000	$0.70 - 0.79 \times a_1 \times a_2$	$0.84 - 0.85 \times a_1 \times a_2$	$1.14 - 0.81 \times a_1 \times a_2$
	1500	$0.72 - 2.50 \times a_1 \times a_2$	$0.89 - 2.60 \times a_1 \times a_2$	$1.25 - 2.60 \times a_1 \times a_2$
H2	750	$0.70 - 0.08 \times a_1 \times a_2$	$0.79 - 0.21 \times a_1 \times a_2$	1.00
	1000	$0.76 - 1.00 \times a_1 \times a_2$	$0.87 - 1.40 \times a_1 \times a_2$	$1.12 - 1.30 \times a_1 \times a_2$
	1500	$0.83 - 4.10 \times a_1 \times a_2$	$0.96 - 4.60 \times a_1 \times a_2$	$1.25 - 4.20 \times a_1 \times a_2$
H3	750	0.76	$0.81 - 0.06 \times a_1 \times a_2$	1.00
	1000	$0.83 - 1.20 \times a_1 \times a_2$	$0.90 - 1.36 \times a_1 \times a_2$	$1.11 - 1.30 \times a_1 \times a_2$
	1500	$0.93 - 4.70 \times a_1 \times a_2$	$1.00 - 4.80 \times a_1 \times a_2$	$1.27 - 5.10 \times a_1 \times a_2$
H4	750	0.78	0.83	1.00
	1000	0.85	$0.91 - 1.60 \times a_1 \times a_2$	$1.10 - 2.40 \times a_1 \times a_2$
	1500	$0.97 - 10.0 \times a_1 \times a_2$	$1.03 - 12.5 \times a_1 \times a_2$	$1.27 - 14.0 \times a_1 \times a_2$
B2	750	$0.66 - 0.09 \times a_1 \times a_2$	$0.77 - 0.14 \times a_1 \times a_2$	1.00
	1000	$0.69 - 0.70 \times a_1 \times a_2$	$0.81 - 0.77 \times a_1 \times a_2$	$1.08 - 0.64 \times a_1 \times a_2$
	1500	$0.74 - 3.20 \times a_1 \times a_2$	$0.88 - 3.30 \times a_1 \times a_2$	$1.20 - 2.90 \times a_1 \times a_2$
B3	750	0.73	$0.80 - 0.05 \times a_1 \times a_2$	1.00
	1000	$0.79 - 0.63 \times a_1 \times a_2$	$0.87 - 0.81 \times a_1 \times a_2$	$1.10 - 0.73 \times a_1 \times a_2$
	1500	$0.86 - 2.40 \times a_1 \times a_2$	$0.95 - 2.60 \times a_1 \times a_2$	$1.23 - 2.80 \times a_1 \times a_2$
B4	750	0.77	0.82	1.00
	1000	0.83	0.88	$1.09 - 0.29 \times a_1 \times a_2$
	1500	$0.92 - 1.70 \times a_1 \times a_2$	$0.99 - 2.20 \times a_1 \times a_2$	$1.24 - 2.60 \times a_1 \times a_2$

For factor $f_9 < 0.5$, please refer to us!

Table 8 Thermal capacity factor for gear units with fan f10				
Gear unit type	n 1/min	Place of installation		
		Small confined spaces Wind velocity ≥ 0.5 m/s	Large halls, workshops Wind velocity ≥ 1.4 m/s	In the open Wind velocity ≥ 4.0 m/s
H1	750	$0.97 - 0.05 \times a_1 \times a_2$	$0.97 - 0.04 \times a_1 \times a_2$	1.00
	1000	$1.18 - 0.33 \times a_1 \times a_2$	$1.20 - 0.33 \times a_1 \times a_2$	$1.23 - 0.32 \times a_1 \times a_2$
	1500	$1.53 - 1.00 \times a_1 \times a_2$	$1.53 - 0.95 \times a_1 \times a_2$	$1.56 - 0.94 \times a_1 \times a_2$
H2	750	$0.95 - 0.07 \times a_1 \times a_2$	$0.96 - 0.06 \times a_1 \times a_2$	1.00
	1000	$1.16 - 0.65 \times a_1 \times a_2$	$1.17 - 0.63 \times a_1 \times a_2$	$1.21 - 0.55 \times a_1 \times a_2$
	1500	$1.54 - 2.40 \times a_1 \times a_2$	$1.55 - 2.40 \times a_1 \times a_2$	$1.58 - 2.20 \times a_1 \times a_2$
H3	750	$0.89 - 0.29 \times a_1 \times a_2$	$0.91 - 0.25 \times a_1 \times a_2$	1.00
	1000	$1.06 - 1.30 \times a_1 \times a_2$	$1.08 - 1.20 \times a_1 \times a_2$	$1.17 - 0.93 \times a_1 \times a_2$
	1500	$1.38 - 4.20 \times a_1 \times a_2$	$1.40 - 4.10 \times a_1 \times a_2$	$1.48 - 3.70 \times a_1 \times a_2$
B2	750	0.95	0.96	1.00
	1000	$1.13 - 0.15 \times a_1 \times a_2$	$1.14 - 0.16 \times a_1 \times a_2$	$1.19 - 0.19 \times a_1 \times a_2$
	1500	$1.47 - 0.95 \times a_1 \times a_2$	$1.48 - 0.92 \times a_1 \times a_2$	$1.52 - 0.95 \times a_1 \times a_2$
B3	750	0.94	0.96	1.00
	1000	$1.13 - 0.17 \times a_1 \times a_2$	$1.14 - 0.18 \times a_1 \times a_2$	$1.18 - 0.25 \times a_1 \times a_2$
	1500	$1.48 - 1.40 \times a_1 \times a_2$	$1.49 - 1.40 \times a_1 \times a_2$	$1.52 - 1.40 \times a_1 \times a_2$

For factor $f_{10} < 0.5$, please refer to us!

"*" On request.

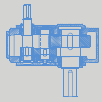


Table 9 Thermal capacity factor for gear units with cooling coil f_{11}				
Gear unit type	n 1/min	Place of installation		
		Small confined spaces Wind velocity ≥ 0.5 m/s	Large halls, workshops Wind velocity ≥ 1.4 m/s	In the open Wind velocity ≥ 4.0 m/s
H1	750	0.87	0.91	1.00
	1000	$0.97 - 0.02 \times a_1 \times a_2$	$1.03 - 0.05 \times a_1 \times a_2$	$1.16 - 0.10 \times a_1 \times a_2$
	1500	$1.15 - 0.19 \times a_1 \times a_2$	$1.22 - 0.23 \times a_1 \times a_2$	$1.39 - 0.33 \times a_1 \times a_2$
H2	750	0.88	0.91	1.00
	1000	1.01	$1.06 - 0.08 \times a_1 \times a_2$	$1.17 - 0.24 \times a_1 \times a_2$
	1500	$1.27 - 0.79 \times a_1 \times a_2$	$1.33 - 0.88 \times a_1 \times a_2$	$1.47 - 1.10 \times a_1 \times a_2$
H3	750	0.89	0.91	1.00
	1000	1.04	1.07	$1.18 - 0.38 \times a_1 \times a_2$
	1500	$1.38 - 0.78 \times a_1 \times a_2$	$1.34 - 1.10 \times a_1 \times a_2$	$1.47 - 1.60 \times a_1 \times a_2$
B2	750	0.86	0.90	1.00
	1000	0.98	1.02	$1.15 - 0.09 \times a_1 \times a_2$
	1500	1.14	$1.19 - 0.05 \times a_1 \times a_2$	$1.38 - 0.37 \times a_1 \times a_2$
B3	750	0.88	0.91	1.00
	1000	1.03	1.06	$1.17 - 0.18 \times a_1 \times a_2$
	1500	$1.28 - 0.35 \times a_1 \times a_2$	$1.32 - 0.48 \times a_1 \times a_2$	$1.46 - 0.84 \times a_1 \times a_2$

For factor $f_{11} < 0.5$, please refer to us!

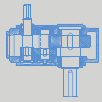
Table 10 Thermal capacity factor for gear units with fan and cooling coil f_{12}				
Gear unit type	n 1/min	Place of installation		
		Small confined spaces Wind velocity ≥ 0.5 m/s	Large halls, workshops Wind velocity ≥ 1.4 m/s	In the open Wind velocity ≥ 4.0 m/s
H1	750	0.98	0.98	1.00
	1000	$1.19 - 0.09 \times a_1 \times a_2$	$1.20 - 0.09 \times a_1 \times a_2$	$1.22 - 0.09 \times a_1 \times a_2$
	1500	$1.56 - 0.31 \times a_1 \times a_2$	$1.56 - 0.30 \times a_1 \times a_2$	$1.57 - 0.29 \times a_1 \times a_2$
H2	750	0.97	0.98	1.00
	1000	$1.19 - 0.25 \times a_1 \times a_2$	$1.20 - 0.25 \times a_1 \times a_2$	$1.22 - 0.25 \times a_1 \times a_2$
	1500	$1.59 - 1.06 \times a_1 \times a_2$	$1.59 - 1.00 \times a_1 \times a_2$	$1.61 - 1.00 \times a_1 \times a_2$
H3	750	0.94	0.95	1.00
	1000	$1.14 - 0.46 \times a_1 \times a_2$	$1.15 - 0.47 \times a_1 \times a_2$	$1.20 - 0.48 \times a_1 \times a_2$
	1500	$1.51 - 2.10 \times a_1 \times a_2$	$1.52 - 2.00 \times a_1 \times a_2$	$1.57 - 2.00 \times a_1 \times a_2$
B2	750	0.97	0.98	1.00
	1000	$1.17 - 0.08 \times a_1 \times a_2$	$1.18 - 0.08 \times a_1 \times a_2$	$1.21 - 0.12 \times a_1 \times a_2$
	1500	$1.55 - 0.47 \times a_1 \times a_2$	$1.55 - 0.47 \times a_1 \times a_2$	$1.58 - 0.52 \times a_1 \times a_2$
B3	750	0.97	0.97	1.00
	1000	$1.17 - 0.08 \times a_1 \times a_2$	$1.18 - 0.10 \times a_1 \times a_2$	$1.21 - 0.19 \times a_1 \times a_2$
	1500	$1.56 - 0.84 \times a_1 \times a_2$	$1.57 - 0.85 \times a_1 \times a_2$	$1.60 - 0.92 \times a_1 \times a_2$

For factor $f_{12} < 0.5$, please refer to us!

Table 11 Size factor a_1												
Size	3	4	5	6	7	8	9	10	11	12	13	14
a_1	0.024	0.030	0.050	0.055	0.065	0.075	0.085	0.095	0.135	0.160	0.190	0.200
Size	15	16	17	18	19	20	21	22	23	24	25	26
a_1	0.270	0.290	0.320	0.345	0.370	0.390	0.530	0.610	Please refer to us.			

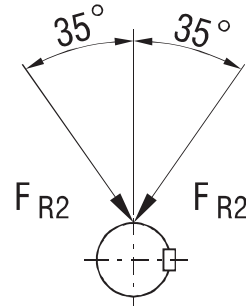
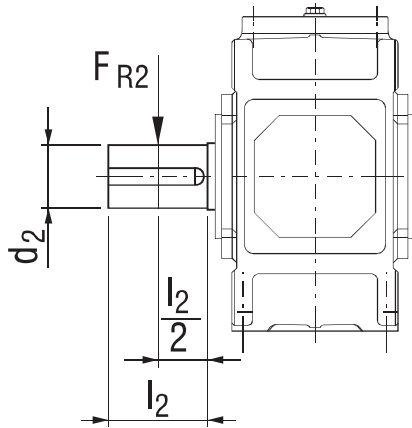
Table 12 Transmission ratio factor a_2													
i	H1SH	i	H2SH	i	H3SH	i	H4SH	i	B2SH	i	B3SH	i	B4SH
1.25	13.000	6.3	1.800	22.4	0.320	100	0.020	5	3.500	12.5	0.950	80	0.110
1.4	12.000	7.1	1.600	25	0.310	112	0.015	5.6	2.800	14	0.850	90	0.100
1.6	10.000	8	1.400	28	0.270	125	0.012	6.3	2.400	16	0.800	100	0.090
1.8	8.500	9	1.100	31.5	0.230	140	0.009	7.1	1.900	18	0.750	112	0.080
2	8.000	10	0.890	35.5	0.190	160	0.007	8	1.600	20	0.700	125	0.070
2.24	7.000	11.2	0.740	40	0.170	180	0.004	9	1.350	22.4	0.650	140	0.060
2.5	6.500	12.5	0.630	45	0.160	200	0.002	10	1.200	25	0.550	160	0.050
2.8	6.000	14	0.530	50	0.110	224	0	11.2	1.100	28	0.450	180	0.040
3.15	3.500	16	0.450	56	0.080	250	0	12.5	0.950	31.5	0.380	200	0.030
3.55	3.300	18	0.370	63	0.050	280	0	14	0.850	35.5	0.330	224	0.020
4	2.900	20	0.330	71	0.045	315	0	16	0.800	40	0.300	250	0.010
4.5	2.100	22.4	0.320	80	0.040	355	0	18	0.750	45	0.270	280	0
5	1.600	25	0.310	90	0.035	400	0			50	0.200	315	0
5.6	1.600	28	0.270	100	0.020	450	0			56	0.150	355	0
				112	0.015					63	0.130	400	0
										71	0.120		
										80	0.110		
										90	0.100		

Note: Gear units installed in open field will avoid direct sunshine by equipping a shelter.



Permissible Additional Radial Forces on Output Shaft:

Permissible Additional Radial Forces on Output Shaft d2



Permissible direction of force

Permissible additional radial forces F_{R2} in kN with application of force on centre of shaft end

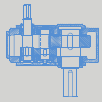
Type	Design	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
H1SH	A/B	*	—	*	—	*	—	*	—	*	—	*	—	*	—	*	—
H2S.	A/B/G/H	—	10	22	22	30	30	30	45	64	64	150	150	140	205	205	205
	C/D	—	10	13	13	18	18	10	28	35	35	112	112	85	135	135	135
H3S.	A/B/G/H	—	—	29	29	40	40	40	60	85	85	190	190	185	265	265	265
	C/D	—	—	18	18	26	26	18	40	50	50	150	150	120	185	185	190
H4S.	A/B	—	—	—	—	26	26	18	40	50	50	150	150	120	185	185	190
	C/D	—	—	—	—	40	40	40	60	85	85	190	190	185	265	265	265
B2S.	A/C	—	13	27	27	37	37	38	55	78	78	160	160	150	210	210	210
	B/D	—	12	15	15	17	17	10	30	35	38	110	110	75	145	100	100
B3S.	A/C	—	14	29	29	40	40	40	60	85	85	190	190	185	265	265	265
	B/D	—	9	18	18	26	26	18	40	50	50	150	150	120	185	185	190
B4S.	A/C	—	—	29	29	40	40	40	60	85	85	190	190	185	265	265	265
	B/D	—	—	18	18	26	26	18	40	50	50	150	150	120	185	185	190

Note: 1) Values in tables are minimum values. If the angle of application of force and the direction of rotation are given, significantly higher additional forces can mostly be allowed. Please consult us.

2)* On request.

3)**For application of force outside the centre of the shaft end, see P216.

4) Use foundation bolts of min. property class 8.8. Foundation must be dry and grease-free. Permissible additional radial forces on input shaft d1 on request.



Permissible Additional Radial Forces on Output Shaft d2

Application of force outside the centre of the shaft end

$$F_{RZ2} = F_{R2} \times k$$

F_{RZ2} Permissible external radial force

F_{R2} Permissible additional radial force acc. to table

k Factor of application of force acc. to table

Factor of application of force k															
Size	Distance z (mm)														
	- 200	- 150	- 100	- 75	- 50	- 25	0	25	50	75	100	150	200	250	300
3					1.21	1.09	1.00	0.85	0.74	0.65	0.58	0.48			
4					1.17	1.08	1.00	0.86	0.76	0.68	0.62	0.52	0.44		
5、 6				1.22	1.14	1.06	1.00	0.88	0.79	0.72	0.66	0.56	0.49	0.43	
7、 8				1.19	1.12	1.06	1.00	0.89	0.81	0.74	0.68	0.58	0.51	0.46	0.41
9、 10			1.22	1.15	1.10	1.05	1.00	0.90	0.82	0.76	0.70	0.61	0.54	0.48	0.44
11、 12			1.18	1.13	1.08	1.04	1.00	0.91	0.84	0.78	0.73	0.64	0.57	0.51	0.47
13、 14		1.24	1.15	1.11	1.07	1.03	1.00	0.92	0.86	0.80	0.75	0.67	0.60	0.55	0.50
15、 16		1.20	1.12	1.09	1.06	1.03	1.00	0.93	0.87	0.82	0.77	0.69	0.63	0.58	0.53
17、 18	1.25	1.17	1.11	1.08	1.05	1.03	1.00	0.94	0.88	0.84	0.79	0.72	0.66	0.60	0.56

HB